

## <u>Regulate a 0 to 500V, 10-mA power supply in</u> <u>a different way</u>

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Contemporary power supplies use switching techniques to achieve the desired output voltage from the primary source. Switching power supplies, however, are often too noisy to be used in sensitive analog circuits. You may find linear power supplies to be preferable in these cases.

A standard practice for a linear voltage regulator is shown in **Figure 1**. A higher-than-desired, unstable voltage is connected to the input,  $V_{IN}$ , and the series-pass transistor,  $Q_1$ , reduces the voltage to the desired level at output  $V_{OUT}$ . An error amplifier, IC<sub>1</sub>, compares a fraction of  $V_{OUT}$  with a reference voltage,  $V_{R}$ , and controls  $Q_1$  to keep the output fixed regardless of the load current,  $I_{OUT}$ , and variations of  $V_{IN}$ . Such a circuit is suitable only for a small range of output voltages.



Figure 1 A standard linear voltage regulator connects the feedback directly to the series-pass transistor,  $Q_1$ .

When a wide range of output settings is desired, as in laboratory power supplies, the value of resistor  $R_{Q1}$  must be small enough to allow sufficient base current for transistor  $Q_1$  at the high end of the output voltage range, but excessive power is dissipated at this resistor and transistor  $Q_3$  when output voltage is reduced. Additionally,  $Q_3$  must withstand the maximum  $V_{IN}$ .

You can use the circuit in **Figure 2** to overcome these problems. Two standard transformers,  $T_1$  and  $T_2$  (220V ac to 6V ac, 10W), are used to make an isolated replica of the mains supply,  $V_M$ . This replica is doubled and rectified using  $D_1$ ,  $D_2$ ,  $C_1$ , and  $C_2$  to get about 560V at  $V_{IN}$  from 220V ac at  $V_M$ . As in the standard **Figure 1** connection, a series-pass transistor,  $Q_1$  (BU508A), is used to reduce the unstable  $V_{IN}$  down to a fixed  $V_{OUT}$ , and  $IC_1$  compares the divided  $V_{OUT}$  with  $V_R$ . Potentiometer  $R_3$  sets  $V_R$  to allow for the adjustment of  $V_{OUT}$ , as given by the following **equation**:  $V_{OUT}=V_R\times[(R_{FG}+R_F)/R_{FG}]$ ,

where  $R_F = R_{F1} + R_{F2} \dots R_{Fn}$ .



Figure 2 Optical coupling isolates the high voltage at  $Q_1$  from the op-amp output.

With 10 resistors (1 M $\Omega$  each) connected in series to form  $R_F$  and a maximum reference voltage of 5V, the output voltage can be set from 0 to 505V. The <u>OPA364</u> operational amplifier is a rail-to-rail input type to allow proper operation, with  $V_R$  ranging from 0 to 5V, and is able to source a current of up to 40 mA.

To reduce the power dissipation caused by driving a series-pass transistor and expand the output voltage range, the driving of transistor  $Q_1$  is done in an unconventional way using optical isolation. Two photodiodes,  $FD_1$  and  $FD_2$ , operating in photovoltaic mode, provide the driving current for the base of transistor  $Q_1$ . Light falling on the photodiodes causes a current flow into the base of  $Q_1$ .

The maximum voltage from a single photodiode working in photovoltaic mode is not sufficient to drive the base; therefore, two photodiodes are connected in series. Photodiodes for infrared light at 870 to 950 nm are used, and two IR LEDs,  $LD_1$  and  $LD_2$ , illuminate them. The LEDs are standard 5-mm, plastic-encapsulated types. To improve the transfer ratio of the current through the LED versus the current generated by the photodiode, cut off the tops of the LEDs and polish them to form a flat surface. Place the photodiodes in proximity to the surfaces obtained. The transfer ratio of this homemade optocoupler is about 0.05. (The current of 20 mA through the LED causes a current of 1 mA through the photodiode.) Alternatively, you can use a commercially available linear optocoupler—for example, an IL300, which houses two photodiodes. Its current transfer ratio is only about 0.007, so you should use several such components in parallel.

The current-limiting circuit formed by  $Q_2$  and  $R_2$  simply shorts the FD<sub>1</sub> and FD<sub>2</sub> photodiodes when the output current exceeds  $Q_2$ 's turn-on threshold, and the limit is independent of the output voltage. Capacitor C<sub>6</sub> is added for compensation, and transistor  $Q_1$  should be fitted with a heat sink of at least



 $5^{\circ}$ C/W. The power supply for the operational amplifier and the reference voltage is provided from the ac signal between the two transformers using bridge rectifier BR<sub>1</sub> (50V, 1A); two filtering

capacitors,  $C_7$  and  $C_8$ ; and voltage regulator IC<sub>2</sub> (LM7805). A shutdown of the output voltage can be made by a simple short circuit across capacitor  $C_5$ , making  $V_R$  equal to 0.

Those living in a 110V ac region can use locally available transformers, but they should modify the circuit to achieve 500V by adding yet another transformer,  $T_3$  (the same as  $T_1$  and  $T_2$ , all 110V ac to 6V ac, 10W), in such a way that the low-voltage windings are connected in parallel, while the high-voltage windings of transformers  $T_2$  and  $T_3$  are connected in series. The operation of the high-voltage windings can be verified using an ac voltmeter; if the voltmeter reads zero, the ends of the windings from  $T_3$  must be exchanged. Alternatively, if a 220V/6V transformer is available, keep  $T_2$  as 220V/6V and use 110V/6V at  $T_1$ .

**Editor's note:** High voltages of 500V and the available current of several milliamps can be lethal; exercise caution when building, testing, and using this circuit.