

LMC6482 CMOS Dual Rail-To-Rail Input and Output Operational Amplifier

General Description

The LMC6482 provides a common-mode range that extends to both supply rails. This rail-to-rail performance combined with excellent accuracy, due to a high CMRR, makes it unique among rail-to-rail input amplifiers.

It is ideal for systems, such as data acquisition, that require a large input signal range. The LMC6482 is also an excellent upgrade for circuits using limited common-mode range amplifiers such as the TLC272 and TLC277.

Maximum dynamic signal range is assured in low voltage and single supply systems by the LMC6482's rail-to-rail output swing. The LMC6482's rail-to-rail output swing is guaranteed for loads down to 600Ω .

Guaranteed low voltage characteristics and low power dissipation make the LMC6482 especially well-suited for batteryoperated systems.

See the LMC6484 data sheet for a Quad CMOS operational amplifier with these same features.

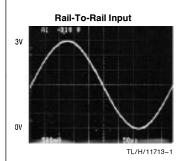
Features (Typical unless otherwise noted)

- Rail-to-Rail Input Common-Mode Voltage Range (Guaranteed Over Temperature)
- Rail-to-Rail Output Swing (within 20 mV of supply rail, 100 kΩ load)
- Guaranteed 3V, 5V and 15V Performance
- Excellent CMRR and PSRR
- Ultra Low Input Current
- High Voltage Gain (R_L = 500 kΩ)
- Specified for 2 kΩ and 600Ω loads

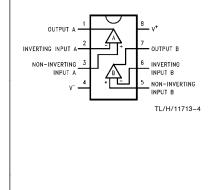
Applications

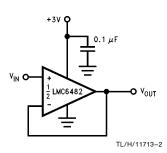
- Data Acquisition Systems
- Transducer Amplifiers
- Hand-held Analytic Instruments
- Medical Instrumentation
- Active Filter, Peak Detector, Sample and Hold, pH Meter, Current Source
- Improved Replacement for TLC272, TLC277

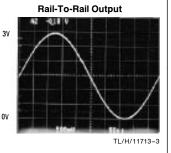




Connection Diagram







Ordering Information

	Temperatu	NSC	Transport		
Package	Military −55°C to +125°C	Industrial - 40°C to + 85°C	Drawing	Media	
8-Pin Molded DIP	LMC6482MN	LMC6482AIN LMC6482IN	N08E	Rail	
8-pin Small Outline		LMC6482AIM LMC6482IM	M08A	Rail Tape and Reel	
8-pin Ceramic DIP	LMC6482AMJ/883		J08A	Rail	

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_MC6482 CMOS Dual Rail-To-Rail Input and Output Operational Amplifier

March 1995

82 dB

20 fA

130 dB

Absolute Maximum Ratings (Note 1)

If Military/Aerospace specified devices are required, please contact the National Semiconductor Sales Office/Distributors for availability and specifications. ESD Tolerance (Note 2) 1.5 kV

Operating Ratings (Note 1)

Supply Voltage	$3.0V \leq V+ \leq 15.5V$
Junction Temperature Range LMC6482AM LMC6482AI, LMC6482I	$\begin{array}{l} -55^{\circ}C \leq T_{J} \leq +125^{\circ}C \\ -40^{\circ}C \leq T_{J} \leq +85^{\circ}C \end{array}$
Thermal Resistance ($ heta_{JA}$) N Package, 8-Pin Molded DIP M Package, 8-Pin Surface Mount	90°C/W 155°C/W

DC Electrical Characteristics

Differential Input Voltage

Voltage at Input/Output Pin Supply Voltage ($V^+ - V^-$)

Current at Input Pin (Note 12)

Current at Power Supply Pin

Storage Temperature Range Junction Temperature (Note 4)

Current at Output Pin (Notes 3, 8)

Lead Temperature (Soldering, 10 sec.)

Unless otherwise specified, all limits guaranteed for $T_J = 25^{\circ}C$, $V^+ = 5V$, $V^- = 0V$, $V_{CM} = V_O = V^+/2$ and $R_L > 1M$. Boldface limits apply at the temperature extremes.

 \pm Supply Voltage

-65°C to +150°C

16V

 $\pm 5 \text{ mA}$

 \pm 30 mA

40 mA

260°C

150°C

 (V^+) +0.3V, (V^-) -0.3V

Symbol	Parameter	Cond	litions	Typ (Note 5)	LMC6482AI Limit (Note 6)	LMC6482I Limit (Note 6)	LMC6482M Limit (Note 6)	Units	
V _{OS}	Input Offset Voltage			0.11	0.750 1.35	3.0 3.7	3.0 3.8	mV max	
TCV _{OS}	Input Offset Voltage Average Drift			1.0				μV/°C	
Ι _Β	Input Current	(Note 13)		0.02	4.0	4.0	10.0	pA max	
l _{OS}	Input Offset Current	(Note 13)		0.01	2.0	2.0	5.0	pA max	
C _{IN}	Common-Mode Input Capacitance			3				pF	
R _{IN}	Input Resistance			>10				$Tera\Omega$	
CMRR	Common Mode Rejection Ratio	$\begin{array}{l} 0V \leq V_{CM} \leq 15.0 \\ V^+ = 15V \end{array}$	0V	82	70 67	65 62	65 60	dB	
		$\label{eq:VCM} \begin{array}{ c c } 0V \leq V_{CM} \leq 5.0 \\ V^+ = 5V \end{array}$	V	82	70 67	65 62	65 60	min	
+ PSRR	Positive Power Supply Rejection Ratio	$\begin{array}{l} 5V \leq V^+ \leq 15V, \\ V_O = 2.5V \end{array}$, V ⁻ = 0V	82	70 67	65 62	65 60	dB min	
-PSRR	Negative Power Supply Rejection Ratio	$\begin{array}{l} -5V \leq V^{-} \leq -15V, V^{+} = 0V \\ V_{O} = -2.5V \end{array}$		82	70 67	65 62	65 60	dB min	
V _{CM}	Input Common-Mode Voltage Range	$V^+ = 5V$ and 15 For CMRR ≥ 50		V ⁻ - 0.3	- 0.25 0	- 0.25 0	- 0.25 0	V max	
				V ⁺ + 0.3V	V ⁺ + 0.25 V ⁺	V ⁺ + 0.25 V ⁺	V ⁺ + 0.25 V ⁺	V min	
A _V	Large Signal Voltage Gain	$R_{L} = 2 k\Omega$ (Notes 7, 13)	Sourcing	666	140 84	120 72	120 60	V/mV min	
			Sinking	75	35 20	35 20	35 18	V/mV min	
		R _L = 600Ω (Notes 7, 13)	Sourcing	300	80 48	50 30	50 25	V/mV min	
			Sinking	35	20 13	15 10	15 8	V/mV min	

Symbol	Parameter	Conditions	Typ (Note 5)	LMC6482AI Limit (Note 6)	LMC6482I Limit (Note 6)	LMC6482M Limit (Note 6)	Units
V _O	Output Swing	$V^+ = 5V$ $R_L = 2 k\Omega$ to $V^+/2$	4.9	4.8 4.7	4.8 4.7	4.8 4.7	V min
			0.1	0.18 0.24	0.18 0.24	0.18 0.24	V max
		$V^+ = 5V$ R _L = 600 \Omega to V ⁺ /2	4.7	4.5 4.24	4.5 4.24	4.5 4.24	V min
			0.3	0.5 0.65	0.5 0.65	0.5 0.65	V max
		$V^+ = 15V$ $R_L = 2 k\Omega$ to $V^+/2$	14.7	14.4 14.2	14.4 14.2	14.4 14.2	V min
			0.16	0.32 0.45	0.32 0.45	0.32 0.45	V max
		$V^+ = 15V$ R _L = 600 \Omega to V ⁺ /2	14.1	13.4 13.0	13.4 13.0	13.4 13.0	V min
			0.5	1.0 1.3	1.0 1.3	1.0 1.3	V max
I _{SC}	Output Short Circuit Current	Sourcing, $V_{O} = 0V$	20	16 12	16 12	16 10	mA min
	$V^+ = 5V$	Sinking, $V_{O} = 5V$	15	11 9.5	11 9.5	11 8.0	mA min
I _{SC}	Output Short Circuit Current	Sourcing, $V_O = 0V$	30	28 22	28 22	28 20	mA min
	V ⁺ = 15V	Sinking, V _O = 12V (Note 8)	30	30 24	30 24	30 22	mA min
IS	Supply Current	Both Amplifiers $V^+ = +5V$, $V_0 = V^+/2$	1.0	1.4 1.8	1.4 1.8	1.4 1.9	mA max
		Both Amplifiers $V^+ = 15V, V_O = V^+/2$	1.3	1.6 1.9	1.6 1.9	1.6 2.0	mA max

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Symbol	Parameter	Conditions	Typ (Note 5)	LMC6482AI Limit (Note 6)	LMC6482I Limit (Note 6)	LMC6482M Limit (Note 6)	Units
SR	Slew Rate	(Note 9)	1.3	1.0 0.7	0.9 0.63	0.9 0.54	V/µs min
GBW	Gain-Bandwidth Product	V ⁺ = 15V	1.5				MHz
φm	Phase Margin		50				Deg
G _m	Gain Margin		15				dB
	Amp-to-Amp Isolation	(Note 10)	150				dB
e _n	Input-Referred Voltage Noise	F = 1 kHz $V_{cm} = 1 \text{ V}$	37				nV/√ ⊦
i _n	Input-Referred Current Noise	F = 1 kHz	0.03				pA/√ ⊦
T.H.D.	Total Harmonic Distortion	$\label{eq:F} \begin{array}{l} F = 10 \; kHz, A_V = -2 \\ R_L = 10 \; k\Omega, V_O = 4.1 \; V_{PP} \end{array}$	0.01				%
		$F = 10 \text{ kHz}, A_V = -2 R_L = 10 \text{ k}\Omega, V_O = 8.5 \text{ V}_{PP} V^+ = 10 \text{ V}$	0.01				%

Symbol	bol Parameter Conditions		Typ (Note 5)	LMC6482AI Limit (Note 6)	LMC6482I Limit (Note 6)	LMC6482M Limit (Note 6)	Units
V _{OS}	Input Offset Voltage		0.9	2.0 2.7	3.0 3.7	3.0 3.8	mV max
TCV _{OS}	Input Offset Voltage Average Drift		2.0				μV/°
IB	Input Bias Current		0.02				pА
los	Input Offset Current		0.01				pА
CMRR	$ \begin{array}{c c} \mbox{RR} & \mbox{Common Mode} & \mbox{OV} \leq V_{\mbox{CM}} \leq 3V \\ \mbox{Rejection Ratio} & \end{array} $		74	64	60	60	dB min
PSRR	Power Supply Rejection Ratio	$3V \le V^+ \le 15V, V^- = 0V$	80	68	60	60	dB min
	Input Common-Mode Voltage Range	For CMRR \geq 50 dB	V ⁻ -0.25	0	0	0	V max
			V ⁺ + 0.25	۷+	۷+	۷+	V min
Vo	Output Swing	$R_L=2k\Omega$ to V+/2	2.8				v
			0.2				V
		$R_L=600\Omega$ to V+/2	2.7	2.5	2.5	2.5	V mir
			0.37	0.6	0.6	0.6	V max
I _S	Supply Current	Both Amplifiers	0.825	1.2 1.5	1.2 1.5	1.2 1.6	mA max
	lectrical Chara otherwise specified, V ⁺	$\begin{array}{c} \textbf{Cteristics} \\ = 3V, V^{-} = 0V, V_{CM} = V_{O} \\ \hline \\ \hline \\ \textbf{Conditions} \end{array}$	= V ⁺ /2, and Typ (Note 5)	R _L > 1M. LMC6482AI Limit (Note 6)	LMC6482I Limit (Note 6)	LMC6482M Limit (Note 6)	Uni
Unless	Parameter		(· ,	. ,		
	Parameter Slew Rate	(Note 11)	0.9				V/µ
Symbol		(Note 11)					V/µ МН
Symbol SR	Slew Rate	(Note 11)	0.9				· ·

Note 8: Do not short circuit output to V⁺, when V⁺ is greater than 13V or reliability will be adversely affected.

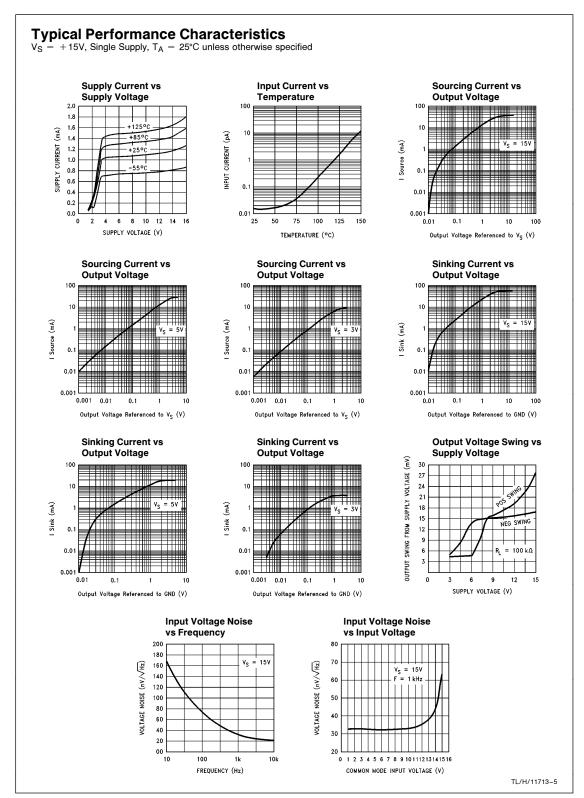
Note 9: V⁺ = 15V. Connected as Voltage Follower with 10V step input. Number specified is the slower of either the positive or negative slew rates.

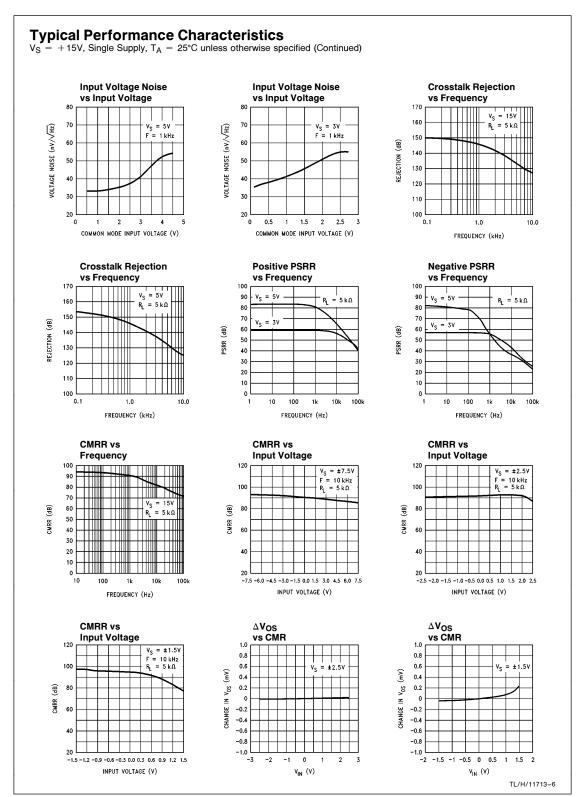
Note 10: Input referred, V $^+$ = 15V and R_L = 100 k Ω connected to 7.5V. Each amp excited in turn with 1 kHz to produce V_O = 12 V_{PP}.

Note 11: Connected as voltage Follower with 2V step input. Number specified is the slower of either the positive or negative slew rates.

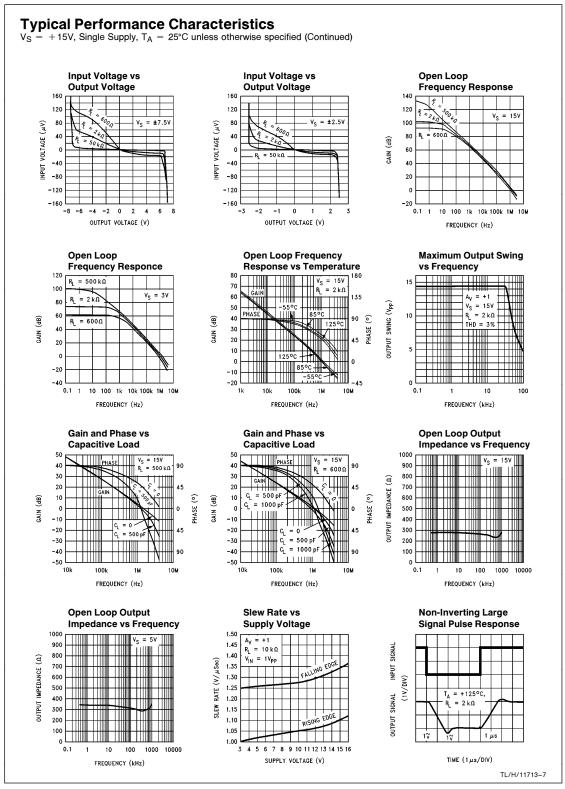
Note 12: Limiting input pin current is only necessary for input voltages that exceed absolute maximum input voltage ratings.

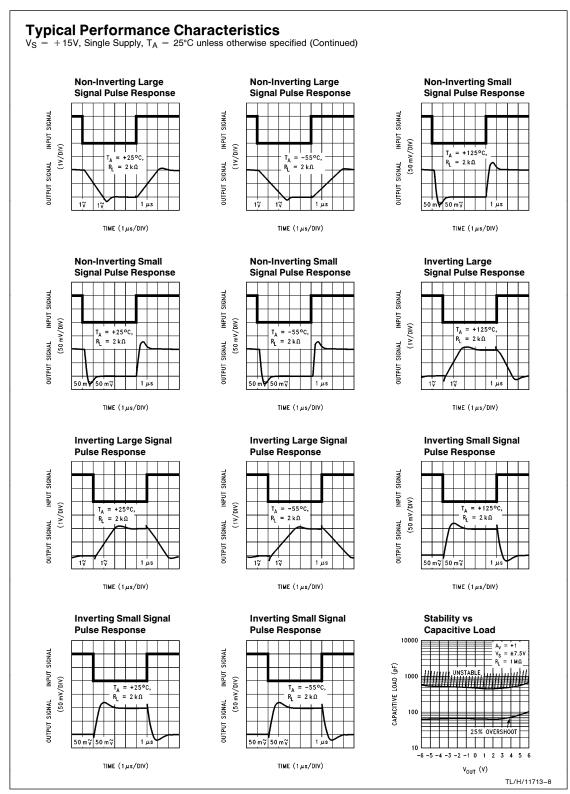
Note 13: Guaranteed limits are dictated by tester limitations and not device performance. Actual performance is reflected in the typical value. Note 14: For guaranteed Military Temperature parameters see RETS6482X.

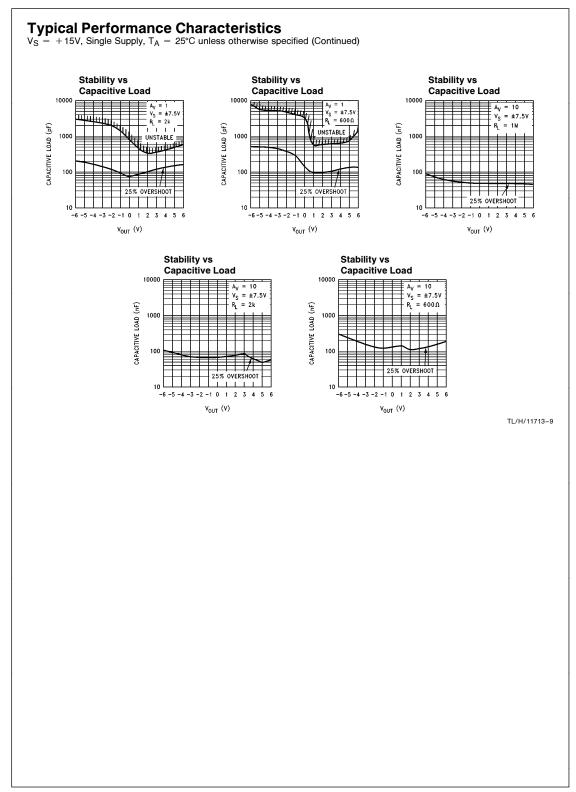












Application Information 1.0 Amplifier Topology

The LMC6482 incorporates specially designed wide-compliance range current mirrors and the body effect to extend input common mode range to each supply rail. Complementary paralleled differential input stages, like the type used in other CMOS and bipolar rail-to-rail input amplifiers, were not used because of their inherent accuracy problems due to CMRR, cross-over distortion, and open-loop gain variation.

The LMC6482's input stage design is complemented by an output stage capable of rail-to-rail output swing even when driving a large load. Rail-to-rail output swing is obtained by taking the output directly from the internal integrator instead of an output buffer stage.

2.0 Input Common-Mode Voltage Range

Unlike Bi-FET amplifier designs, the LMC6482 does not exhibit phase inversion when an input voltage exceeds the negative supply voltage. *Figure 1* shows an input voltage exceeding both supplies with no resulting phase inversion on the output.

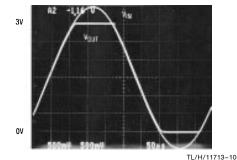


FIGURE 1. An Input Voltage Signal Exceeds the LMC6482 Power Supply Voltages with No Output Phase Inversion

The absolute maximum input voltage is 300 mV beyond either supply rail at room temperature. Voltages greatly exceeding this absolute maximum rating, as in *Figure 2*, can cause excessive current to flow in or out of the input pins possibly affecting reliability.

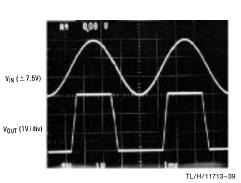
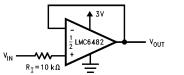


FIGURE 2. A \pm 7.5V Input Signal Greatly Exceeds the 3V Supply in *Figure 3* Causing No Phase Inversion Due to R_I

Applications that exceed this rating must externally limit the maximum input current to ± 5 mA with an input resistor (R_I) as shown in *Figure 3*.



TL/H/11713-11 FIGURE 3. RI Input Current Protection for Voltages Exceeding the Supply Voltages

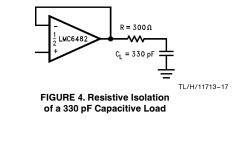
3.0 Rail-To-Rail Output

The approximated output resistance of the LMC6482 is 180Ω sourcing and 130Ω sinking at Vs = 3V and 110Ω sourcing and 80Ω sinking at Vs = 5V. Using the calculated output resistance, maximum output voltage swing can be estimated as a function of load.

4.0 Capacitive Load Tolerance

The LMC6482 can typically directly drive a 100 pF load with $V_S=15V$ at unity gain without oscillating. The unity gain follower is the most sensitive configuration. Direct capacitive loading reduces the phase margin of op-amps. The combination of the op-amp's output impedance and the capacitive load induces phase lag. This results in either an underdamped pulse response or oscillation.

Capacitive load compensation can be accomplished using resistive isolation as shown in *Figure 4*. This simple technique is useful for isolating the capacitive inputs of multiplexers and A/D converters.



Application Information (Continued)

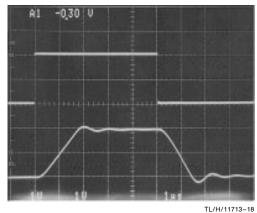
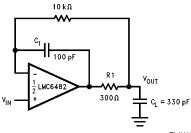


FIGURE 5. Pulse Response of the LMC6482 Circuit in *Figure 4*

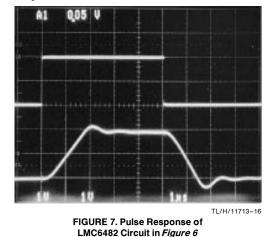
Improved frequency response is achieved by indirectly driving capacitive loads, as shown in *Figure 6*.



TL/H/11713-15

FIGURE 6. LMC6482 Noninverting Amplifier, Compensated to Handle a 330 pF Capacitive Load

R1 and C1 serve to counteract the loss of phase margin by feeding forward the high frequency component of the output signal back to the amplifiers inverting input, thereby preserving phase margin in the overall feedback loop. The values of R1 and C1 are experimentally determined for the desired pulse response. The resulting pulse response can be seen in *Figure 7*.



5.0 Compensating for Input Capacitance

It is quite common to use large values of feedback resistance with amplifiers that have ultra-low input current, like the LMC6482. Large feedback resistors can react with small values of input capacitance due to transducers, photodiodes, and circuits board parasitics to reduce phase margins.

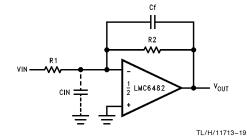


FIGURE 8. Canceling the Effect of Input Capacitance

The effect of input capacitance can be compensated for by adding a feedback capacitor. The feedback capacitor (as in *Figure 8*), C_{f_1} is first estimated by:

$$\frac{1}{2\pi R_1 C_{IN}} \ge \frac{1}{2\pi R_2 C_f}$$

or

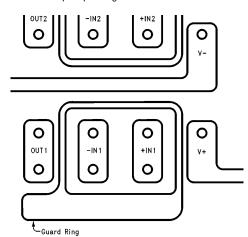
$$\text{R}_1\,\text{C}_{IN} \leq \text{R}_2\,\text{C}_f$$

which typically provides significant overcompensation. Printed circuit board stray capacitance may be larger or smaller than that of a bread-board, so the actual optimum value for C_f may be different. The values of C_f should be checked on the actual circuit. (Refer to the LMC660 quad CMOS amplifier data sheet for a more detailed discussion.)

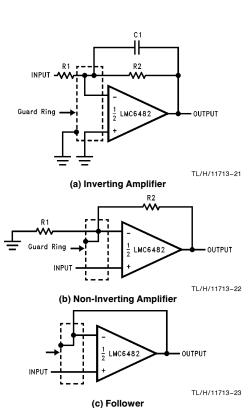
Application Information (Continued) 6.0 Printed-Circuit-Board Layout for High-Impedance Work

It is generally recognized that any circuit which must operrate with less than 1000 pA of leakage current requires special layout of the PC board. When one wishes to take advantage of the ultra-low input current of the LMC6482, typically less than 20 fA, it is essential to have an excellent layout. Fortunately, the techniques of obtaining low leakages are quite simple. First, the user must not ignore the surface leakage of the PC board, even through it may sometimes appear acceptably low, because under conditions of high humidity or dust or contamination, the surface leakage will be appreciable.

To minimize the effect of any surface leakage, lay out a ring of foil completely surrounding the LM6482's inputs and the terminals of capacitors, diodes, conductors, resistors, relay terminals, etc. connected to the op-amp's inputs, as in Figure 9. To have a significant effect, guard rings should be placed on both the top and bottom of the PC board. This PC foil must then be connected to a voltage which is at the same voltage as the amplifier inputs, since no leakage current can flow between two points at the same potential. For example, a PC board trace-to-pad resistance of $10^{12}\Omega$, which is normally considered a very large resistance, could leak 5 pA if the trace were a 5V bus adjacent to the pad of the input. This would cause a 250 times degradation from the LMC6482's actual performance. However, if a guard ring is held within 5 mV of the inputs, then even a resistance of $10^{11}\Omega$ would cause only 0.05 pA of leakage current. See Figures 10a, 10b, 10c for typical connections of guard rings for standard op-amp configurations.

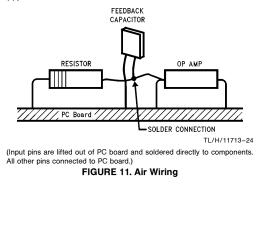






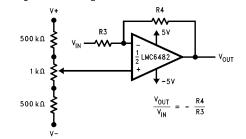


The designer should be aware that when it is inappropriate to lay out a PC board for the sake of just a few circuits, there is another technique which is even better than a guard ring on a PC board: Don't insert the amplifier's input pin into the board at all, but bend it up in the air and use only air as an insulator. Air is an excellent insulator. In this case you may have to forego some of the advantages of PC board construction, but the advantages are sometimes well worth the effort of using point-to-point up-in-the-air wiring. See *Figure* 11.

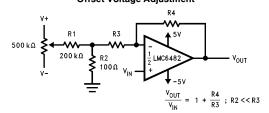


Application Information (Continued) 7.0 Offset Voltage Adjustment

Offset voltage adjustment circuits are illustrated in *Figure 12* and *13*. Large value resistances and potentiometers are used to reduce power consumption while providing typically ± 2.5 mV of adjustment range, referred to the input, for both configurations with V_S = ± 5 V.



TL/H/11713-25 FIGURE 12. Inverting Configuration Offset Voltage Adjustment



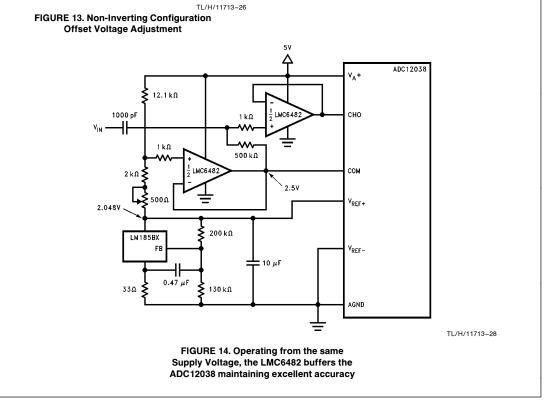
8.0 Upgrading Applications The LMC6484 quads and LMC6482 duals have industry

standard pin outs to retrofit existing applications. System performance can be greatly increased by the LMC6482's features. The key benefit of designing in the LMC6482 is increased linear signal range. Most op-amps have limited input common mode ranges. Signals that exceed this range generate a non-linear output response that persists long after the input signal returns to the common mode range.

Linear signal range is vital in applications such as filters where signal peaking can exceed input common mode ranges resulting in output phase inverison or severe distortion.

9.0 Data Acquisition Systems

Low power, single supply data acquisition system solutions are provided by buffering the ADC12038 with the LMC6482 (*Figure 14*). Capable of using the full supply range, the LMC6482 does not require input signals to be scaled down to meet limited common mode voltage ranges. The LMC4282 CMRR of 82 dB maintains integral linearity of a 12-bit data acquisition system to \pm 0.325 LSB. Other rail-to-rail input amplifiers with only 50 dB of CMRR will degrade the accuracy of the data acquisition system to only 8 bits.



Application Information (Continued)

10.0 Instrumentation Circuits

The LMC6482 has the high input impedance, large common-mode range and high CMRR needed for designing instrumentation circuits. Instrumentation circuits designed with the LMC6482 can reject a larger range of commonmode signals than most in-amps. This makes instrumentation circuits designed with the LMC6482 an excellent choice of noisy or industrial environments. Other applications that benefit from these features include analytic medical instruments, magnetic field detectors, gas detectors, and siliconbased tranducers.

A small valued potentiometer is used in series with R_g to set the differential gain of the 3 op-amp instrumentation circuit in *Figure 15*. This combination is used instead of one large valued potentiometer to increase gain trim accuracy and reduce error due to vibration.

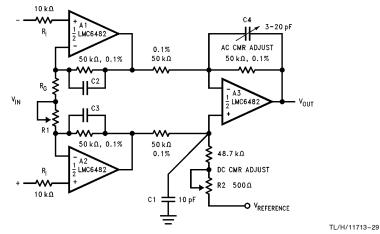


FIGURE 15. Low Power 3 Op-Amp Instrumentation Amplifier

A 2 op-amp instrumentation amplifier designed for a gain of 100 is shown in *Figure 16*. Low sensitivity trimming is made for offset voltage, CMRR and gain. Low cost and low power consumption are the main advantages of this two op-amp circuit.

Higher frequency and larger common-mode range applications are best facilitated by a three op-amp instrumentation amplifier.

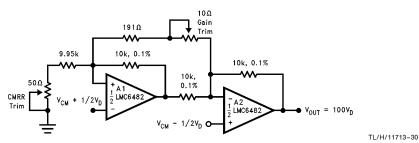


FIGURE 16. Low-Power Two-Op-Amp Instrumentation Amplifier

Application Information (Continued) 11.0 Spice Macromodel

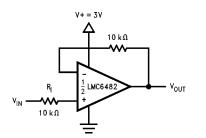
A spice macromodel is available for the LMC6482. This model includes accurate simulation of:

- Input common-mode voltage range
- Frequency and transient response
- GBW dependence on loading conditions
- Quiescent and dynamic supply current
- Output swing dependence on loading conditions

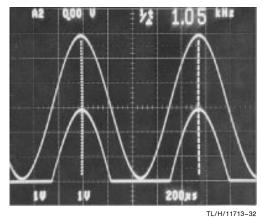
and many more characteristics as listed on the macromodel disk.

Contact your local National Semiconductor sales office to obtain an operational amplifier spice model library disk.

Typical Single-Supply Applications









The circuit in *Figure 17* uses a single supply to half wave rectify a sinusoid centered about ground. R_I limits current into the amplifier caused by the input voltage exceeding the supply voltage. Full wave rectification is provided by the circuit in *Figure 18*.

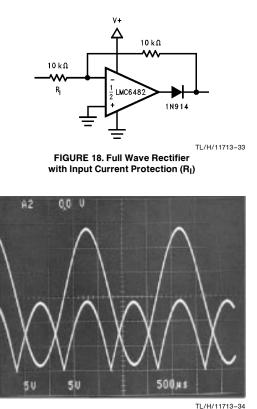


FIGURE 18A. Full Wave Rectifier Waveform

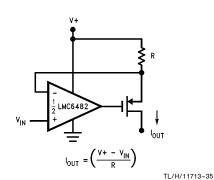
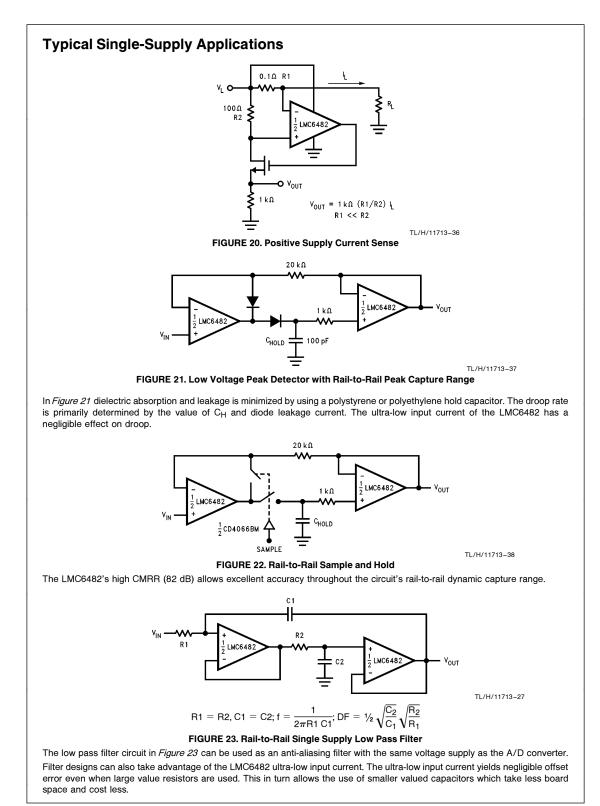
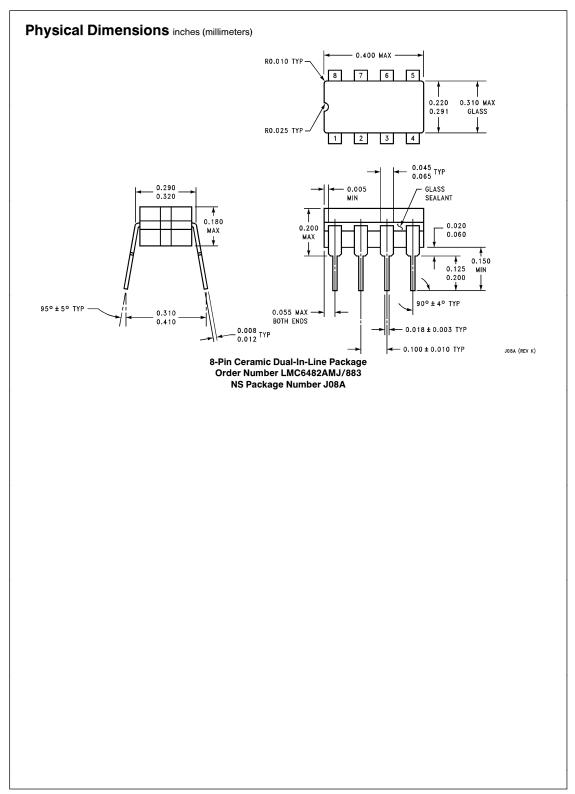
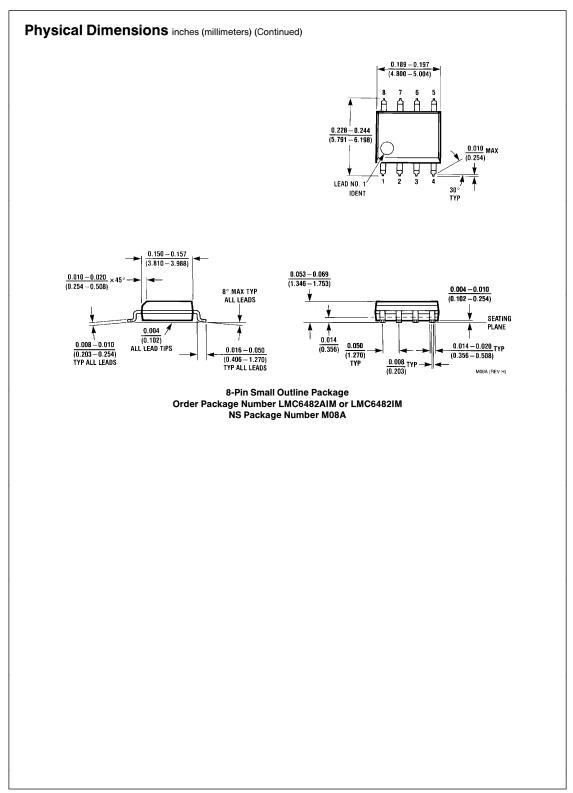
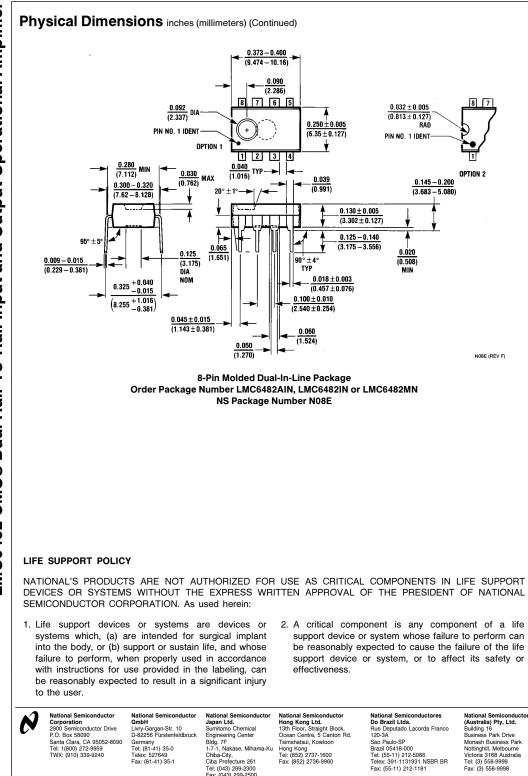


FIGURE 19. Large Compliance Range Current Source









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