

Figure 3.4 Electrical model of an oscilloscope probe.

back to their source. The self-inductance of the ground loop, represented in series inductance L_1 , impedes these currents. How does the inductance L_1 affect our measurements? The reactance of L_1 , working in parallel with the impedance of the probe input, has a finite rise time. We will calculate the 10–90% rise time, and then discuss its significance.

Calculating Ground Loop Inductance

The dimensions of the ground loop in Figure 3.4 are 1 in. × 3 in. A typical ground wire of probe is American Wire Gauge (AWG) 24, having a diameter of 0.02 in. The inductance formula from Appendix C for the case of a rectangular loop is

$$L \approx 10.16 \left[1 \ln \left(\frac{2 \times 3}{0.02} \right) + 3 \ln \left(\frac{2 \times 1}{0.02} \right) \right] \text{ nH} \tag{3.9}$$

$$\approx 200 \text{ nH}$$

Calculating the 10–90% Rise Time

The time constant for this circuit is

$$C = 10 \text{ pF}$$

$$L = 200 \text{ nH}$$

$$T_{LC} = (LC)^{1/2} = 1.4 \text{ ns} \tag{3.10}$$

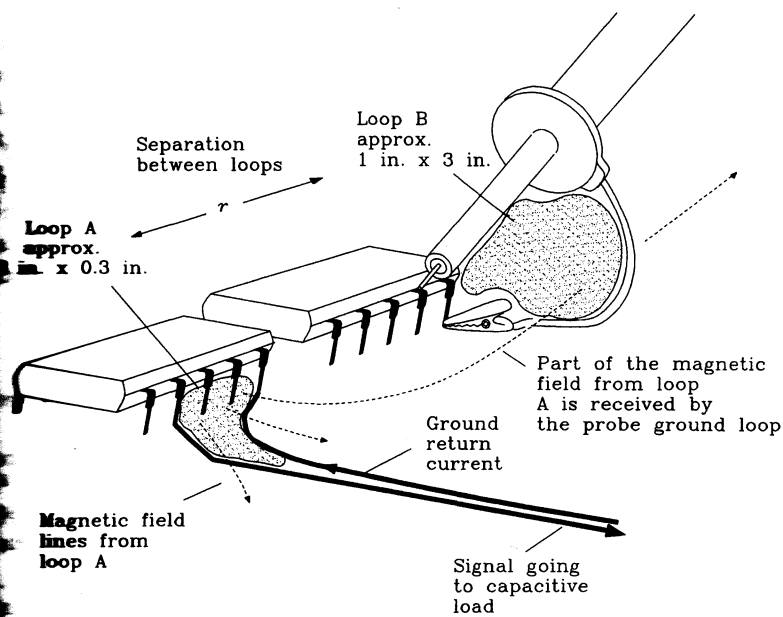


Figure 3.9 A probe ground loop picks up spurious noise voltages.

Mutual Inductance of Loops A and B

The dimensions for loops A and B appear in Figure 3.9, and so we need only apply the formula in Appendix C for the mutual inductance of two loops.

$$L_M = 5.08 \frac{A_1 A_2}{r^3} \tag{3.18}$$

$$= 5.08 \frac{(0.3 \times 0.3)(1 \times 3)}{2^3} \tag{3.19}$$

$$= 0.17 \text{ nH} \tag{3.20}$$

where A_1 = area of loop 1, in.²

A_2 = area of loop 2, in.²

r = separation of loops, in.

L_M = mutual inductance between loops 1 and 2, H

Induced Voltage by the Definition of Mutual Inductance

The voltage induced in loop B is the product of the rate of change in current in loop A and the mutual inductance of loops A and B:

$$V_{\text{noise}} = L_M \frac{dI}{dt} = (0.17 \text{ nH})(7.0 \times 10^7 \text{ V/s}) = 12 \text{ mV} \tag{3.21}$$

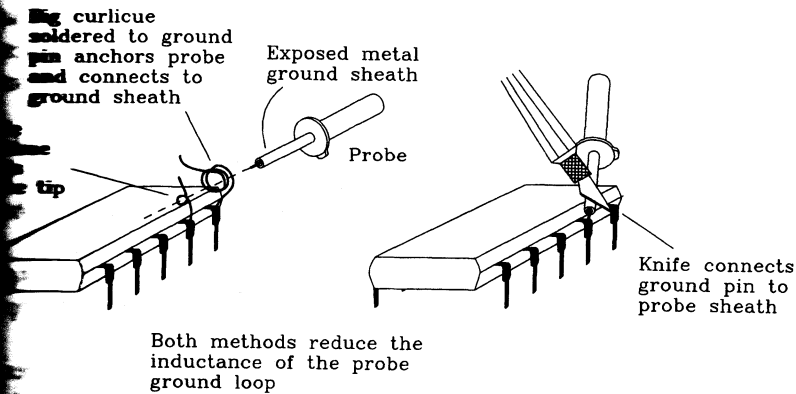


Figure 3.8 Methods for grounding a probe tip near a signal under test.

the knife blade method? Table 3.1 lists the 10–90% rise time in nanoseconds as a function of the ground loop inductance for both TTL (30-Ω) and ECL (10-Ω) circuits.

TABLE 3.1 EFFECT OF GROUND LOOP INDUCTANCE ON 10- AND 2-pF PROBE PERFORMANCE

Ground loop inductance (nH)	10-pF probe			2-pF probe		
	T_{10-90}	Q_{TTL}	Q_{ECL}	T_{10-90}	Q_{TTL}	Q_{ECL}
200	2.8	4.7	14.1	1.3	10.5	32.0
100	2.0	3.3	9.9	0.89	7.4	22.0
30	1.1	1.8	5.4	0.49	4.1	12.0
10	0.6	1.1	3.2	0.28	2.4	7.1
3	0.3	0.6	1.7	0.15	1.3	3.9
1	0.2	0.3	1.0	0.09	0.7	2.2

For a 10-pF probe, we would have to get the loop inductance down below 10 nH to achieve acceptable overshoot performance on TTL rise times of 1 ns. For ECL circuits, we would need an even lower inductance.

To reduce loop inductance, let's try replacing the ground wire in Figure 3.4 with a thicker wire. If the original wire was AWG 24, we can try AWG 18, which has a diameter of 1.02 mm. Reworking Equation 3.9 for this new ground lead,

$$L \approx 10.16 [1 \ln(3/0.02) + 3 \ln(1/0.02)] \text{ nH} \quad [3.16]$$

$$\approx 170 \text{ nH} \quad [3.17]$$

How slowly inductance changes as a function of wire diameter? Doubling the diameter in this case makes only a 15% change in inductance. The slow variation in